

1 **The Multi-Speed Deflectometer: New technology developed for traffic-**
2 **speed non-destructive structural testing of pavements.**

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11 **ABSTRACT.** The Traffic Speed Deflectometer has transformed pavement structural data
12 collection on highways, where network testing was formerly carried out with Falling Weight
13 Deflectometer, Deflectograph or Beam. However, the Multi-Speed Deflectometer (MSD) is now
14 also available, which can test highways but more significantly, fills a gap for an efficient device
15 for structural testing of urban roads. In these locations, issues that are often overlooked include
16 the frequent slowing or stopping at intersections, cornering, access, the extreme variability of
17 structural stiffness due to pavement subservices and the collection of quality structural data over
18 a wide range of speeds while still ensuring the unimpeded flow of traffic at all times. The Multi-
19 Speed Deflectometer is an economical non-destructive traffic speed pavement testing device used
20 to benchmark the structural capacity of large networks of roads. Data are collected at 1m intervals,
21 usually in both wheelpaths and averaged to 10 or 20m intervals in each lane. MSD structural data
22 have been collected over the last 4 years in multiple regions throughout New Zealand and Italy.
23 When paired with traditional surface profiling from the high-speed data (HSD), reliable traffic
24 records and maintenance history, a comprehensive understanding of the mechanisms of pavement
25 performance can be achieved including both the surfacing and the structural layers. Examples are
26 provided to demonstrate application. Pavements with a poor surface condition can be cross
27 checked against the structural condition to verify whether there is an underlying structural issue.
28 If so, these sites can then be flagged for project level testing and renewal. Sites with poor surfacing
29 condition and no structural issues can be flagged for maintenance or re-surfacing treatment. The
30 right solution for the right problem at the right time and over the right extents can now be
31 economically identified, providing authorities with the capability of assessing the optimum Net
32 Present Value expenditure for any large roading network.

33
34 **Keywords.** Multi-Speed Deflectometer, pavement deflections, structural evaluation, non-
35 destructive testing
36

37 **Introduction**

38 The Traffic Speed Deflectometer (Zofka and Sudyka, 2015; Xiao et al., 2021) has transformed
39 pavement structural data collection particularly because standard reporting at 10m intervals or
40 less addresses the extreme variability of structural stiffness inherent in many pavements.
41 However, its cost and the limited number of units worldwide means it is not always readily
42 available for pavement screening. Traditionally, the Falling Weight Deflectometer (Ullidtz, 1998)
43 has been used for both network and project level surveying in many countries worldwide. While
44 FWD testing has proven extremely useful to confirm the distress mode and most effective type
45 of rehabilitation design at project level, it is much less effective for network level surveying
46 because it is slow and hence often is used with low test density (points per road area coverage).
47 Furthermore, the FWD requires costly traffic management to minimise health and safety risks to
48 the operators and road users. Similar limitations are associated with other traditional devices, such
49 as the Deflectograph and Benkelman Beam.

50 The Multi-Speed Deflectometer (MSD) is now also available, which can test highways
51 but also fills a gap for an efficient device for structural testing of urban roads where access,
52 cornering, frequent reductions in speed with stopping at intersections, and the collection of quality
53 structural data over a wide range of customary traffic speeds, are important considerations. The
54 Multi-Speed Deflectometer is ideal for economical non-destructive traffic speed pavement
55 structural testing in these conditions to benchmark the structural capacity of a large network of
56 roads. Data are recorded at 1m intervals, usually in both wheel tracks (300,000 test points per
57 day) and averaged to 10 or 20m, providing near continuous structural data useful for defining
58 structurally homogenous sections and to indicate the location of reduced capacity within the
59 pavement cross section i.e., which pavement layer will first develop distress and hence become
60 critical.

61 Network level pavement management based solely on surface condition observations
62 relies on identifying distress only once it manifests. Additional structural testing is required to
63 identify the cause of distress, because assessment from surface parameters enables only short-
64 term Forward Works Programming (1 to 2 years), hence inhibiting the planned intervention prior
65 to the initiation of distress reaching a terminal condition. Most of the traditional surface condition
66 parameters (rutting, roughness, cracking and visual imaging) can be collected simultaneously
67 with the same MSD vehicle, greatly reducing the overall cost and carbon emissions for provision
68 of comprehensive state-of-the-art network management.

70 **Comparison of TSD, FWD and MSD**

71 The science underlying FWD and TSD is limited to recording of vertical velocity of the pavement
72 surface at unloaded points near a heavy uniaxial load on a plate (FWD) or between moving wheels
73 (TSD), whereas the science underlying the MSD involves capturing all forms of 3-dimensional
74 deformation of the pavement surface using multiple sensors and images recording data both from
75 beneath and around the contact patches of heavily loaded moving wheels. Differences between
76 the FWD and MSD are compared in detail in Table 1.

77 The measures are fundamentally different, but it is important to note that all of the
78 differences are such that the MSD deformations are more representative of the actual in situ
79 deformations that occur under a heavy vehicle. Therefore, the deformations from the MSD should
80 be more suitable for predicting pavement performance particularly where there are multiple
81 distress modes, or where models that acknowledge only uniform layers with vertical loading are

82 less appropriate. ASTM D5858 (2020) highlights the issues involved for calculating layer moduli
 83 from FWD test results, particularly for cracked pavements or locations without pavement layering
 84 information.

85 The use of lasers on the TSD limits surveys to drier conditions which in the case of New
 86 Zealand surveys and limited TSD availability has led to avoidance of testing in wet seasons when
 87 pavements are in their most susceptible condition. The MSD can survey in both wet and dry
 88 conditions and because a dedicated vehicle is not required (installation of the various devices
 89 takes only a few hours), multiple MSDs can be readily mobilised and available, including in
 90 remote locations.

91
 92 Table 1. Key Differences between the MSD and FWD

Multi Speed Deflectometer	Falling Weight Deflectometer
Pneumatic tyre (deformable) with 30mm rubber and steel mesh/ply	Steel/fibre circular plate (stiff) covered with 3mm of ribbed rubber
Rolling load creating a mini “bow wave” at traffic speed	Stationary position and weights dropped to mimic vertical load at traffic speeds
Rotation of principal stresses	Fixed orientation of principal stresses
Measurement of 3D longitudinal, transverse and vertical deformations characterising the asymmetric deflection bowl	Measurement of vertical deformations only, characterising a symmetric deflection bowl
Transverse accelerations affect wheel load to match those of actual heavy vehicles	No consideration of any transverse (radial) accelerations on corners or due to camber or superelevation
Using a rolling wheel inherently acknowledges that the longitudinal profile (at all wavelengths) induces changes in dynamic vertical loads which have a consequent impact on pavement life prediction.	Static location provides a reading which relates only to loading from a smooth road (IRI=0). <i>This leads to both under and over prediction of remaining structural life, and substantially so for mature roads</i>
Near continuous spatial coverage at about 1m centres optionally presented as median each 10 or 20m	Spatially separated individual test points every 20 or 50m centres staggered across lanes –no indication of variation on the vast majority of the pavement
Both wheeltracks tested simultaneously at minimal additional cost.	Normally only one wheel track is tested, otherwise costs are double. Data collection and traffic management can be difficult when surveying the offside wheel path
Response is always from loading within each wheeltrack as no additional edge clearance is required.	As the FWD load plate is centrally located, the wheelpath cannot always be tested if there is inadequate clearance (eg from parked vehicles)

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 94
 95 ASTM D4695-03 (2020) General Pavement Deflection Measurements also includes
 96 FWD testing intervals according to the different goals, ranging from an upper limit of 500m for
 97 network level, reducing to 10m where necessary for detailed project level. These limitations do
 98 not apply to the MSD given the continuous nature of testing.

99
 100 **MSD Design Objectives**

101 The MSD has been developed by installing and exploring the recordings of all types of high
 102 performance sensors and continually upgrading their configuration as available specifications for
 103 these are progressively enhanced. The prime objective is to extend beyond the traditional
 104 limitation (recording only vertical deformation) to more realistically characterise the “myriad
 105 ways” (Dawson, 2002) in which pavements respond when experiencing different modes of
 106 distress. Effectively recording their multi-dimensional dynamic behaviour provides the basis of a

107 more mechanistic approach for performance prediction.

108 MSD vehicles can be supplemented with other sensors (such as GPR & TDR), but these
109 substantially increase the cost/km, yet the consequential effects of their parameters are already
110 incorporated in the primary deformations beneath and around the tyre contact patch as recorded
111 by standard MSD.

112

113 **MSD Data Collection and Rationale for Interpretation**

114 State-of-the-art pavement condition data collection and its structural evaluation requires:

- 115 • Collection of data to be non-destructive at traffic speed (no impediment to road users).
- 116 • Coverage of both the surface of existing roads and where practical, each layer of any road
117 under construction, recording all data, near-continuously from both wheel paths of all
118 appropriate lanes.
- 119 • Processing that determines all parameters relevant to pavement performance in a manner
120 that also enables mechanistic characterisation.
- 121 • Identification of all modes of distress in all layers.
- 122 • Characterisation of spatial and temporal maintenance or renewal needs (extents, depths,
123 and optimum timing) for each test point.
- 124 • Sub-sectioning all test points into homogenous Structural Treatment Lengths (STL), with
125 ongoing re-sectioning (dynamic incremental-recursive model).
- 126 • Design of the most economic form of maintenance and timing for sub-intervals within
127 each STL, and categorise each for local maintenance versus full length renewal
- 128 • Prediction of Remaining Structural Life, with a usefully reliable “Hit Rate” for each STL
- 129 • Determination of the optimum Forward Work Programmes for both Maintenance and
130 Renewals (with due recognition of their interdependence) and determination of their
131 respective costs.

132 Historically, such evaluations with FWD have been slow, costly and of variable reliability
133 (Arnold et al, 2009). Speed has been greatly increased with the advent of the Traffic Speed
134 Deflectometer, although the length of the TSD makes it impractical on many local authority roads.
135 Now with the Multi-Speed Deflectometer as well, all roads (under construction or completed,
136 surfaced or unsurfaced, dry or wet in any condition) can be tested at traffic speed. MSD provides
137 the additional advantages of measurements where the rubber meets the road (beneath the contact
138 patch not just in the unloaded gap between dual wheels) as well as providing mechanistic insight
139 into 3-dimensional deformations, testing continuously in both wheelpaths. The instrumentation is
140 readily transportable to remote sites and can be installed or adapted to fit most heavy vehicles
141 (including trailers or forklifts). Calibration is carried out using FWD, TSD, (or even
142 Deflectograph or Beam if necessary), initially for seamless transition by their practitioners but
143 ultimately for the more comprehensive characterisation of pavement properties and performance
144 obtainable from the new technology.

145 Since the introduction of non-destructive testing of pavements by A C Benkelman in 1952
146 (Highway Research Board, 1955) until now, the focus has been almost exclusively on one
147 parameter: vertical deflection.

148 The science underlying FWD or TSD is somewhat limited in view of the above. Both
149 devices record only vertical velocity of the pavement surface at unloaded points near a heavy

150 uniaxial load on a plate (FWD) or between moving wheels (TSD). Widely recognised analytical
151 models are then used for quantification of moduli, stresses and strains for known as-built layering.

152 The science underlying the MSD is somewhat different in that it focuses on capturing all
153 forms of 3-dimensional deformation of the pavement surface. The relevant stress/strain tensor
154 field throughout the deflection bowl (with each point having 9 components), and its observed
155 asymmetry beneath a moving wheel precludes using just a simplistic measure (vertical
156 deformation) if pavement life for a network is to be predicted with any reliability (particularly
157 where there is minimal as-built information). Technology now provides a practical option with
158 the capability for much more relevant, more comprehensive and more extensive data collection
159 at traffic speed and at much lesser cost. MSD uses multiple sensors and images recording data
160 both from beneath and around the contact patches of heavily loaded moving wheels then applying
161 primarily machine learning to correlate the large volumes of data with equivalent simple data
162 from an FWD or TSD recording of the same interval of road. Machine learning is then extended
163 to associate other forms of 3-dimensional deformation recorded, using calibrations to sites that
164 have known precedent performance in that region, including those observed to be experiencing
165 specific distress modes or are in a terminal condition. This approach is taken because often there
166 is little or no as-built information and so far, there appears to be no existing analytical model that
167 will:

- 168 (1) interrogate all of the recorded 3-dimensional dynamic characteristics of the deformations
169 induced by a moving wheel and
- 170 (2) output relevant parameters for an asymmetric layered visco-elastic model in a practical
171 timeframe for network structural analysis and
- 172 (3) evaluate them using any existing recognised criteria (fatigue limits).

173 Machine learning provides pavement engineers using MSD with a particularly effective
174 tool to advance this new discipline mechanistically, beyond the limitations of the traditional
175 scientific method, paraphrasing Anderson (2003):

176
177 “This is a world where massive amounts of data can, to a large degree at least, replace
178 every other tool or test that might be brought to bear. Numbers give us not only immediate lessons
179 from relevant history (regional precedent performance), but also unlimited potential for ongoing
180 improvement.

181 Who knows the full theory of why roads perform the way they do? The point is they do,
182 and for every region’s permutation of terrain, sources, practices, loadings and climate, machine
183 learning can now track and quantify their precedent performance with unprecedented fidelity.

184 With enough data, the numbers speak for themselves.”

185

186 Pavements are highly variable structures that are not often amenable to simplistic analysis
187 yet many of the traditional models are uni-variate (sometimes bi-variate). Experience with MSD
188 data from large networks has demonstrated that multi-variate models that give due recognition to
189 the myriad ways in which pavements become distressed, provide more reliable solutions. Many
190 pavement models are based on results from laboratory testing or Accelerated Pavement Test
191 facilities located at great distance from the relevant region. Few practitioners use relevant
192 calibrated models that take into account all of the local conditions; subgrades, aggregate sources,
193 construction methods, maintenance practices, environment etc. Until recently there was little
194 choice. Such regionally-specific, calibrated mechanistic models based on historic observations of
195 all relevant distress modes and precedent performance were often too costly or time-consuming

196 to establish. However, high-speed collection of both structural and surface condition data together
197 with the recent advances in big-data machine learning technology has effectively transformed the
198 industry and provided a choice. Informed pavement management, more reliable performance
199 prediction and optimised planning of forward work have become practical and economic realities
200 for both categories of pavement networks, (highways and local roads).

201 Software has been developed, e.g., Regional Precedent Performance (RPP) which uses
202 multi-variate analysis to analyse these huge data sets providing informed understanding of
203 pavement deterioration and modelling of future performance. The cost is typically orders less than
204 the cost of one kilometre of pavement rehabilitation, and benefits continue for many years.

205 Traditional methodology with visual inspections provides some information on pavement
206 life predictions for up to 1-2 years ahead at best. The MSD provides the potential for a significant
207 step forward that addresses Transport Agency focus on improving longer term predictions i.e.
208 from 30 months out to 30 years. While reliability has been very low to at least until 2010, the
209 potential for better reliability on highways with FWD supplemented by TSD data was indicated
210 more recently by Stevens & Schmitz (2018), and with appropriate MSD output as well this is now
211 being successfully extended to wider networks, including for the first time, local authority roads.
212 Regional Precedent Performance longer term prediction of pavement life (RPP 30-30) is now
213 being targeted with the latest MSD upgrades in hardware, firmware and software.

214 Outputs are now able to be delivered in close to real time, (the same day if necessary)
215 enabling much more cost-effective and timely decision making for construction projects.

216

217 **MSD Outputs**

218 MSD data output comes in three forms with varying detail in their characterisation: Basic,
219 Empirical or Developmental.

220 *Basic MSD Outputs*

221 Basic output is generated simply by correlation to the widely recognised FWD parameters, i.e.
222 central deflection and curvature, standardised to 40kN load by default (50kN if required).
223 Curvature for thick structural surfacings is commonly required as Surface Curvature Index,
224 although where thin surfacings predominate, Curvature Function may be preferred.

225 *Empirical MSD Outputs*

226 Empirical outputs include the HDM IV parameter, Adjusted Structural Number (SNP). In
227 addition, more pertinent indices are available, similar to those promoted in Italy by ANAS (2021)
228 since 2009 and in South Africa by Horak (2008), that focus on which layer is of interest and are
229 determined from vertical deflection bowl offsets (at unloaded locations). Horak uses indices (with
230 units of distance) and suffix of I for Index. To distinguish from these, MSD uses the prefix SN as
231 the range of values is tied to SNP range for the network (normally 0 to 8). The corresponding
232 MSD layer parameters are generated at or near loaded locations and are:

- 233 • Structural Number for Rutting (SNR) reflecting the stiffness of the whole pavement. It
234 is similar to structural number (SNP) and relates inversely to central deflection. SNR
235 relates to the resistance to rutting from the combination of movement in all layers
236 resulting from both vertical and longitudinal deformations, scaled to the same range as
237 SNP. The Structural Number for Vertical deformation (SNV) is also generated, relating
238 to the vertical component of rutting deformation only.

- 239 • Structural Number for Base (SNB) a measure of the strength of the main structural layer
240 and relates inversely to surface curvature index.

241 The above are the principal indices that may be provided for those familiar with FWD,
242 TSD, Deflectograph or Beam, and calibration may be to whichever form of data is most readily
243 available for any individual network.

244 ***Developmental MSD Outputs***

245 The MSD processing also outputs “Developmental” indices which relate to more specific
246 characteristics which are at present recorded only by the MSD or are newly developed or under
247 development (because they can be collected at minimal additional cost with the same vehicle).
248 MSD research began in 2015 and the “signatures” of the multi-dimensional tensor field
249 deformations present an enigma of which about 10% has been able to be deciphered each year,
250 using principally, machine learning calibrations to observed performance. Many of the recorded
251 features are not yet fully understood in relation to the progression of specific distress modes. Note
252 not all of the following developmental indices have yet been advanced to the stage they can be
253 used for production, but are documented here so that longer term goals can be indicated, and
254 others may elect to use them for research (eg by applying them on sites where the reasons for
255 premature distress are unknown but can then be explored by observing whether the extents of
256 distress severity correspond consistently with extreme values). Feedback of this type of
257 information and re-analysis greatly accelerates understanding of the relevant distress
258 mechanisms, and ongoing feedback loops become successively more useful each year especially
259 on heavily trafficked roads, as the significance of the MSD deformations becomes more evident
260 from distress progression on each network. Re-processing to incorporate any changes in distress
261 severity that are observed is fully automated. On most local roads where the traffic loading is
262 reasonably well known or recorded, the structural testing should remain current and not need to
263 be re-tested for several years.

264 Some of the developmental indices can be utilised in lieu of traditional HSD parameters.
265 If HSD data are already available or become available in due course, they should be used in
266 preference, otherwise the interim MSD equivalents may be adopted for network evaluation to
267 refine or guide remaining life algorithms using MSD deformations.

- 268 • Structural Number for the Surface (SNS) a measure of the resistance to near surface
269 instability along the wheelpath. It is significant only occasionally and is relevant to
270 distress in unbound aggregates or thin surfacings.
- 271 • Modular Ratio Index (MRI) is a measure of the ratio of the moduli of successive layers
272 above the subgrade, calibrated to the Normalised Modular Ratio parameter for FWD. A
273 value of 1.0 indicates compaction is likely to be satisfactory and conforming with the
274 Austroads modular ratios expected from good quality unbound granular aggregates.
275 Values less than 1.0 may indicate under-compaction. Significantly higher values
276 indicate bound layers may be present.
- 277 • Structural Number for Transverse Shear. (SNT) is a measure of the resistance to
278 transverse shear. Low values are expected to be relatively rare in full width pavements
279 but occasionally experienced in narrow (rural) thin surfaced unbound granular
280 pavements on low strength shallow subgrade where the outer wheelpath is too close to a
281 soft shoulder, and as a result may be accompanied by deep-seated shear or possibly
282 edge break. There is no closely equivalent parameter in traditional tests using vertical

283 deflection. Interim calibration uses the ratio of the FWD shear strain at the top of the
284 subgrade to the equivalent thickness (as far as the transition only with truncation of
285 values). Beyond the transition, an interim mirror calibration could be attempted, to see
286 what can be learnt. Very low values will suggest subgrade deformation is likely. The
287 intermediate values around the transition are all expected to indicate soundly compacted
288 unbound granular pavements or thick bound layers, that may also relate to high modular
289 ratios. Further trials to find suitable correlations are needed.

- 290 • Bound Cracking Index (BCI) is a new parameter that quantifies the potential for
291 cracking of a near surface bound layer because it is underlain by a significantly more
292 flexible layer. It is correlated to FWD data using pavements that have known
293 construction (usually those with thick AC or cement stabilised basecourses) and known
294 current condition.
- 295 • Apparent Cracking Index (ACI) is generated by MSD as a simplistic measure of
296 cracking from Jpeg images, 300mm square, taken in the wheeltrack at 1 m intervals.
297 Machine learning is used to quantify in real time, just the number of cracks which are
298 essentially continuous ie pass fully from one side to another, returning numbers of 0, 1,
299 2, 3, or 4 with counting truncated at 4. Shorter cracks are ignored.
- 300 • Estimated International Roughness Index (eIRI) and Estimated Mean Texture Depth
301 (eMTD). The estimated descriptions are used to distinguish the parameters from those
302 collected using traditional equipment, as the MSD uses laser imagery to provide
303 localised measures that approximate the traditional International Roughness Index and
304 Mean Texture Depth, both correlated to existing data typically measured by HSD in
305 roading databases such as RAMM (New Zealand).
- 306 • Apparent Rolling Resistance (ARR) is the ratio of the dynamic shear resistance (acting
307 longitudinally on the pavement surface at the tyre contact patch) that is generated
308 against the direction of motion of a free rolling wheel, to the normal force on the
309 pavement, expressed as a percentage. The shear force is the resultant of the forces
310 contributed by tyre deformation (including contact patch hysteresis losses around the
311 patch perimeter as well as internally from texture indentation) and pavement layer
312 deformations (that impose energy losses as the wheel continually attempts to “climb
313 out” of the deflection bowl). The bowl becomes progressively more asymmetric with
314 speed. Because Rolling Resistance has been found to be strongly speed dependent
315 (Cenek, 1996), it is standardised to a reference speed (currently 50 km/hr) as well as
316 other aspects, particularly tyre temperature and pressure. It has associated parameters
317 that allow correction to other vehicle speeds, tyre types and pressures where required. In
318 recent years, Rolling Resistance has been a feature of detailed research in Europe (for
319 identification of pavement types which result in reduction of carbon emissions) using
320 more costly traditional test procedures. However, it was recently discovered that the
321 same parameter was generated incidentally (an unexpected “by product” of the machine
322 learning technology) in the MSD interpretation. For that reason, it may also be
323 outputted when required by interested researchers.

324 The advantage of this extended form of data collection available via MSD is that users
325 may elect either to use simply one or two parameters such as SNP or central deflection, along
326 with traditional HSD data collected separately, or they may elect to encompass the dozen or so
327 supplementary parameters that can now be readily generated in a single MSD pass. In either case,
328 basic interpretation can be limited to dTIMS or Austroads, or extended to include the more
329 versatile tools of a Regional Precedent Performance evaluation and hence Remaining Structural

330 Life and a Forward Work Programme, generated from calibrations to terminal sites in the network
331 – the ultimate reality checks.

332
333 **MSD Case Histories**

334 ***Auckland Transport, Auckland, New Zealand***

335 Over two months in May and June 2021, 4,460 lane
336 km in both left (outer) and right (inner) wheelpaths
337 were collected using MSD data technology on behalf
338 of Auckland Transport. Readings were typically
339 collected at 1 to 3m intervals and reported as the
340 median value of the readings within each 10m road
341 segment. Left and right wheelpath data were
342 staggered. Roads tested comprised mainly arterials
343 and primary collectors. The scale of the data
344 collected over the entire network is best appreciated
345 geospatially as shown in Figure 1.

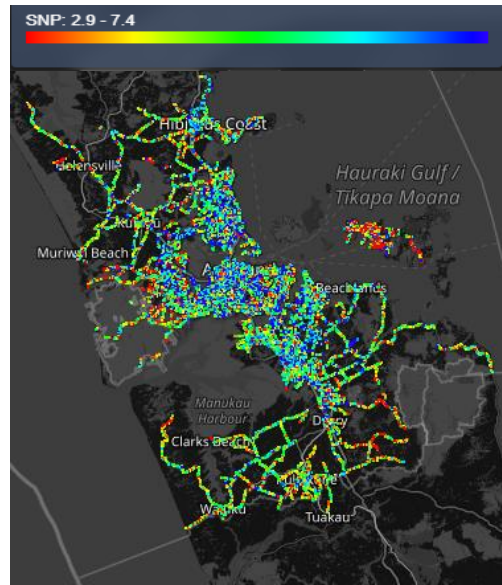
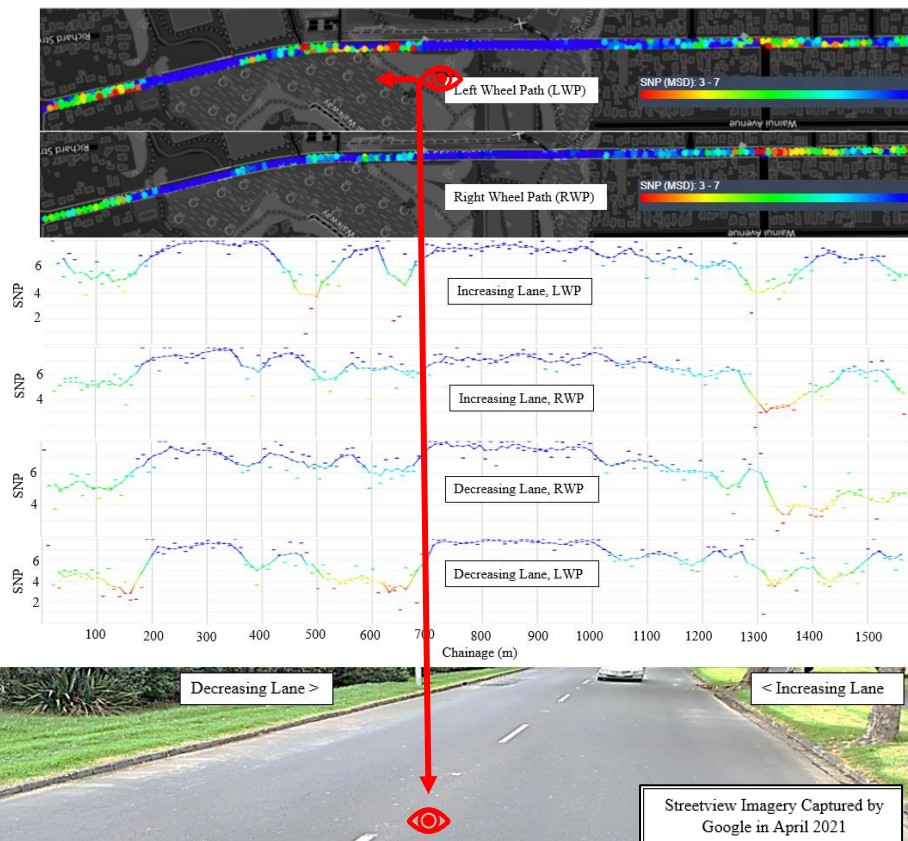


Figure 1. MSD Test coverage for Auckland Transport

346 The final outputs are as per the MSD outputs
347 outlined earlier in the report. Structural Treatment Lengths (section lines in lieu of points) have
348 yet to be determined and reported at time of writing this paper, however their characterisation
349 can at present be readily inferred on inspection as shown in **Error! Reference source not**
350 **found.** for Meola Rd and will in due course be computed algorithmically.
351



352

353

354 Figure 2. Meola Rd, Auckland example of MSD data in all lanes and wheelpaths, well supported by
 355 visual reality checks

356 **Rome Municipality, Rome, Italy**

357 Over three days in April 2021, 300 lane km in the
 358 right (outer) wheel path were collected using MSD
 359 technology. Roads tested mainly comprised
 360 arterials and primary collectors of the municipality
 361 network as shown in Figure 3.

362 Via Prenestina in the vicinity of Villa
 363 Gordiani was selected for closer inspection as
 364 shown in Figure 4. Sub-sections of sustained low
 365 and high SNP were reality checked with Google
 366 Street View Imagery captured in January 2022,
 367 just a few months after MSD testing. Review of
 368 historical imagery indicates that the pavement had
 369 been resurfaced or rehabilitated circa 2015. Within 2-3 years distress manifested at the surface
 370 in the form of fine alligator cracks and pumping. Distress is more severe in the left rather than
 371 right wheelpath highlighting the potential benefit of dual wheelpath MSD surveys particularly
 372 for mature roading networks such as Rome.
 373

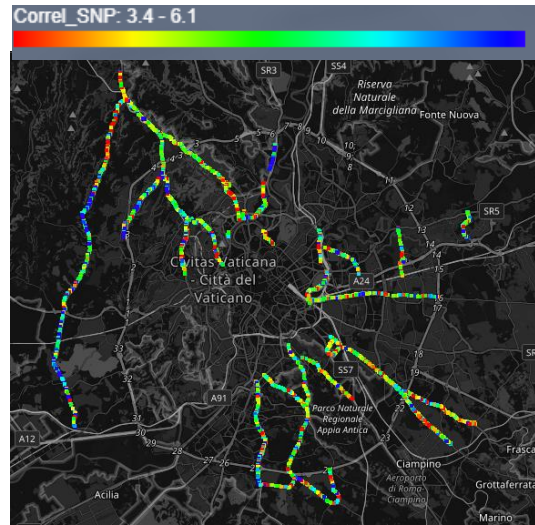


Figure 3. MSD Test coverage for Rome

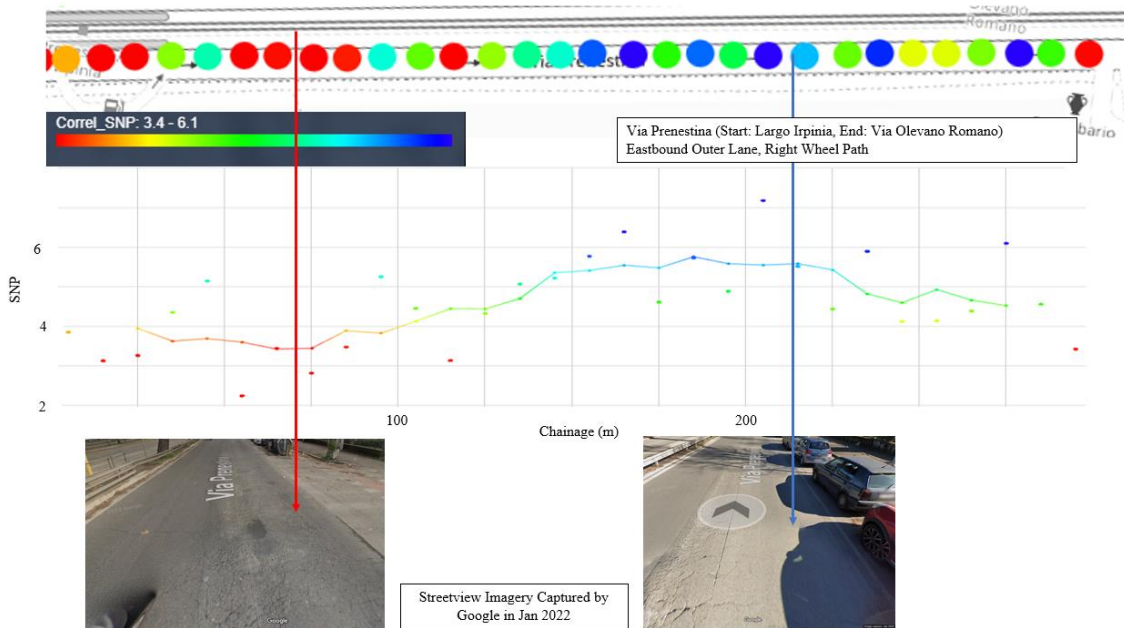


Figure 4. Reality checks on sub-sectioning of Via Prenestina.

374
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376 **Florence Municipality, Florence, Italy**

377 Over three days in December 2021, 185
378 lane km in the right (outer) wheelpath were
379 collected using MSD technology. Roads
380 tested comprised arterials and primary
381 collectors. The scale of the data collected
382 over the entire network is best appreciated
383 geospatially as shown in Figure 5.

384 Viale Francesco Talenti was
385 selected for closer inspection as shown in
386 Figure 6. Sub-sections of sustained
387 low and high SNP were reality checked
388 with Google Street View Imagery captured
389 in January 2022, just a few weeks after
390 MSD testing. Once again the MSD appears
391 to have correlated well with identified sections of weak and strong pavements.
392

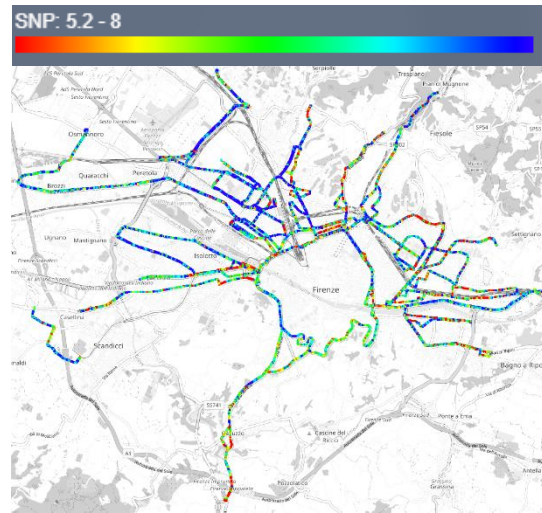


Figure 5. MSD Test coverage for Florence

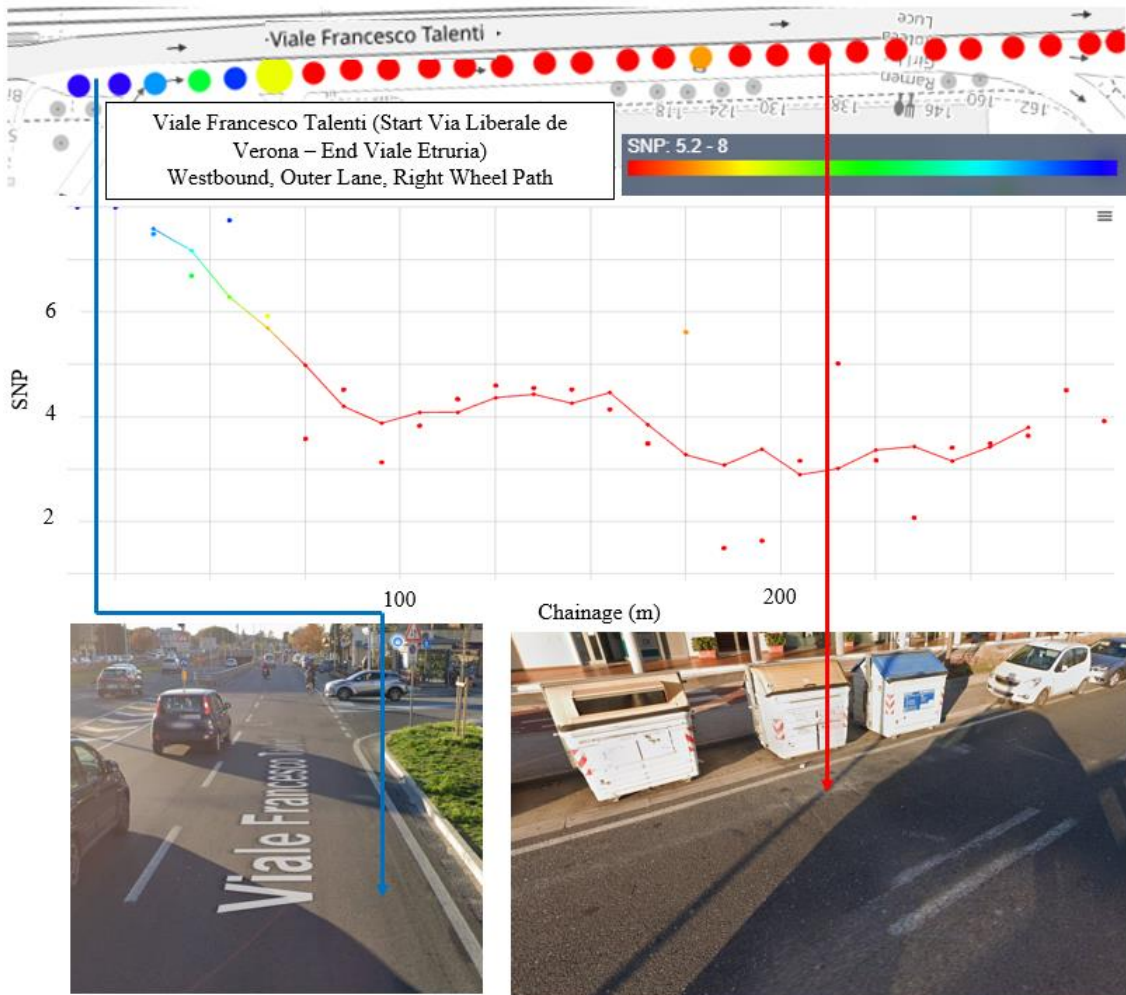


Figure 6. Viale Francesco Talenti Reality Checks

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396 **Conclusions**

397 The Multi-Speed Deflectometer, fills a gap for an efficient device for rapid low-cost testing and
398 structural evaluation of a large network of urban roads. The above recent case histories
399 demonstrate its effectiveness using Google Streetview. Management of pavement deterioration
400 can now be expedited by development of an optimised Forward Works Programme which can
401 be readily validated with traditional methods (visual inspection, destructive tests or minimal
402 Falling Weight Deflectometer testing).

403

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